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A handwritten signature in black ink, appearing to read "Pia Høybye-Olsen".

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Modtaget

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**Method for measuring flow by means
of an ultra sonic flow meter**

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Method for measuring flow by means of an ultra sonic flow meter

The invention concerns a method for measuring flow by use of an ultra sonic flow meter. More specific, the invention is directed to a method of measuring 5 transmission times of, and time difference between, an upstream and a downstream ultra sonic signal.

This time difference is proportional to the flow, and used in time of flight ultra sonic meters as a measure of the flow. If the time difference Δt becomes longer than the duration of the period of the ultra sonic signal, an exact 10 detection of the time difference becomes difficult due to the signal periodicity. In order to avoid this problem, known solutions provide detection circuits that are practically independent of the extent of Δt , i.e. the detection circuit makes measurement possible on ultra sonic flow meters, which have a Δt longer than the period of the signal. An example of such prior art detection method 15 and circuit - also called a trigger - is described in the following, where the envelope of the upstream and downstream signal play a significant role.

The basic purpose of a trigger in a transmit time ultrasonic flow meter is to 20 "point" out the time of arrival of the ultrasonic signal. This is used to measure both the difference between the upstream and downstream transmission time and to measure the two transmission times. From these values the flow Q can be calculated according to (1):

$$(1) \quad Q = k \cdot \frac{\Delta t}{t_1 \cdot t_2}$$

where Δt is the difference time, t_1 and t_2 the transmission times and k a 25 constant dependent on the geometry of the tube. If the media is known, the measurement of the two transmission times can be replaced by measuring the media temperature and calculating the sound speed C from knowledge of the sound speeds variation with temperature:

$$(2) \quad Q = k \cdot \Delta t \cdot C^2$$

where Q is the flow, k is a constant, Δt the time difference and C the sound speed.

Figure 1 is an illustration of the receive signals - the first arriving is the result of the sound pulse travelling in the flow direction, 1, and the second is the result of the sound pulse travelling against the flow direction, 2. In the following the term zero crossing will be used, in practical implementations this will be signal zero (the middle of the range of voltage used in the implementation) or some value either a little over or under the signal zero.

Still referring to Figure 1, the basic problem is to trig or initiate the time measuring circuit with the "same" zero crossing in the upstream and the downstream sound pulse, otherwise a wrong Δt is measured. P_1 and P_2 are to be imagined as same zero crossings because each have a distance of $3\frac{1}{2}$ periods from reception of the sound pulse. Also indicated in the figure is the period t_{sig} of the sound signal and the time difference Δt .

Figure 2 shows how the prior art ultra sonic flowmeter uses the envelope of the ultrasonic signal to achieve a zerocrossing detection, that is independent of the length of Δt . The incoming signal (S_1) is rectified (B_1) and the result is (S_2). This signal (S_2) is feed trough a band pass filter with non-minimum phase behaviour (B_2). (Non-minimum phase systems have the transient property that their initial direction of response is in the opposite direction of the final value - as a consequence, if the filter parameters are chosen appropriately, the output of the filter (B_2) will have a well defined zero crossing indicating the receive time. Furthermore this zero crossing will be independent of the amplitude of the receive signal. The signal on the output of the filter is seen as (S_3). The zero crossing of the signal (S_3) is detected by the zero cross detector (B_3), this signal (S_4) is arming the zero cross detector (B_4). After arming the zero cross detector (B_4), the next positive (- or negative, dependent on the actual implementation) - zero crossing in the original receive signal (S_1) is detected by (B_4) resulting in the signal (S_5).

The time where the signal (S5) changes from low to high is measured relative to the time of the transmit burst (or relative to another time with a known relation to the transmit time). If the time between the zero crossing of S3 and the following zero crossing of S1 is very short, there is a risk of detecting two

5 different zero crossings of S1, due to random noise. To avoid this situation it is detected if the two zero crossings are too close, and if this is the case, the transmit signal is inverted – and hence the receive signal. The consequence of the inverted receive signal is that the previously very short time difference between S3 and S1, is now close to one half period of the receive signal. One

10 can chose to measure transit time on the signal zero crossing (S5) or on the zero crossing of the signal (S4). After having calculated a time as described above for an upstream signal, the same procedure is used on the downstream signal. From these two times, a difference time is established and the flow Q calculated.

15 The described detection method works well in systems were the span of Δt is unknown. This is the case for a general purpose ultra sonic flow meters as the one described above, which are used for a variety of tubes having different diameters. This type of ultra sonic flow meters must be able to cope with a very wide span of Δt . However, in some systems, the span of Δt is

20 limited by fluid velocity and/or the mechanical arrangement of the ultra sonic transducers which means that the ultra sonic converter can be designed according to other and less demanding principles. Such a limitation in Δt is the case, if the two ultra sonic transducers mounted in the tube are very close to each other. It will then be known that Δt e.g. will have a maximum value of

25 e.g. 1 μ s. Further, a drawback of the prior art design described above is the relatively extensive and thus costly use of electronic circuitry. Another weakness of the method is the dependence on a stable signal envelope. If for instance a single pulse in the receive signal has a lower amplitude due to electrical noise or particles/air bubbles in the liquid, the envelope form

30 changes, and consequently a wrong Δt will be calculated.

Based on the foregoing, the object of the invention is to provide a detection method which is realized in a simpler way and with fewer electronic components, and still gives a reliable statement as to the difference in transmission time, Δt .

5 This is achieved with a method according to claim 1. The basic idea of the invention is that of trial and error. During the first series of transmission, multiple transmissions are performed, each transmission consisting of an ultra sonic signal in downstream and upstream direction. The starting time of time measurement in the first series of transmissions is based upon a good
10 estimate of when the incoming ultra sonic pulse arrives. If Δt is inside the reference band, the starting time chosen was ok. If not, a second transmission is launched, but this time the starting time is incremented or decremented by an amount, thus raising the chances of succes. These transmissions are repeated until Δt is inside the reference band. The ideal
15 case is the one in which the initial estimate of the starting time corresponds to the optimum. In this case, only one transmission will be performed. The method is especially applicable in ultra sonic flow meters having small Δt 's. Advantageously, the inventive trigger method makes it possible to dispense with much of the trigger hardware, hereby lowering the cost. Compared to
20 Figure 2, electronic circuits B1 and B2 can be omitted. The method has the further advantage, that it is simple to implement and very robust. Thus, the method is practically independent of signal distortions, because it is based on the detection of zero crossings.

Following the first series of transmissions and having placed Δt within the
25 reference band, a second series of transmissions can be launched. Though the method of using a first series of transmissions suffices to make a correct calculation of Δt and flow Q, an improvement is reached by introducing a second series of transmissions sequentially following the first series. The second series remedy problems of variations in the travel time and thus
30 changed zero crossings of the received ultra sonic signal due to varying

temperatures of the liquid media. The second series of transmissions is repeated until the time period between the starting time and a stopping time of the time measurement is approximately equal to a multiplum (1,2,3..) of half the time period of the ultra sonic signal. However, a full time period of the 5 ultra sonic signal is preferred as reference value. The use of half the time period as reference can be preferred if a time circuit with no unlinearities is used. The idea of this second measure in the inventive method is to keep the average time from the starting time to the stopping time constant, hereby positioning the starting and stopping times in an optimum position 10 independent of temperature changes in the media.

Advantageously, the first and second series of transmissions can be supplemented by a third series, where the starting time is incremented or decremented until a difference between a calculated average transmission 15 value and a reference value is inside a reference band. The reference value is determined as a function of the media temperature, and the temperature is either measured or calculated.

The incrementation or decrementation of the starting signal in the third series of transmissions is preferably done in steps with a resolution in time that approximately corresponds to the period of the received signal. A slight 20 variation in the period of the received signal is normal due to differences in temperature on the transducers, thus +/- 40 kHz on a 1MHz transmitted signal is to be expected, but in practice this has no influence. Thus a resolution departing by a small amount of the period time can be used.

In relation to the first transmission series, the timely resolution used in 25 positioning the starting time corresponds to the timely resolution of a digital control unit.

The time measurements, initiated at the starting time, may be stopped at the first positive or negative zero crossing of the received ultra sonic signal, but this demands the use of fast electronic circuits. It is preferred, that the time 30 measurement is stopped at the first positive zero crossing following a

negative zero crossing of the received ultra sonic signal, because it allows the currents and voltages in the electronics to settle, thus avoiding unlinearities. Of course the order can be changed into stopping on a negative zero crossing following a positive.

- 5 It is preferred, that the starting time in the first transmission in the first series of transmission is a fixed value which may be stored in a memory. The fixed starting time is chosen to start approximately in the middle or in the first half of the receiving train of pulses, which ensures a signal with sufficient amplitude for measuring.
- 10 The reference band of the first series of transmissions is delimited by Δt_{\max} and Δt_{\min} and the width of the band is smaller than the time period of the ultra sonic receive signal. Preferredly, the reference band is narrowed by adding a safety margin to the reference band. The safety margin consists at least of the timely resolution, but may also comprise a duration of a timing noise. By 15 incorporating a safety margin into the reference band, increased stability of the method is achieved.

The invention will now be described on the basis of the figures, where

- 20 Figure 1 is a time-amplitude diagram of an upstream and a downstream signal travelling in a media in a tube and generated by ultrasonic transducers.

Figure 2 shows a prior art detection scheme used for finding Δt .

Figure 3 is a time-pulse diagram according to the invention.

Figure 4 shows the reference band of the time difference Δt according to the invention.

- 25 Figure 5 shows a flow chart according to the invention

Figure 6 is a block diagram of the preferred embodiment of the invention.

The following preferred embodiment describes a trigger scheme, for ultrasonic flow meters used for measuring media with a known relation between the sound speed and the temperature of the media, and in which the difference time, Δt , between signals transmitted upstream and downstream is 5 limited to be within one period, t_{sig} , or less of the received ultrasonic signal (i.e. within approximately $1 \mu s$ for the most commonly applied ultrasonic transducers).

Referring to Fig.3, at both the upstream and downstream receive signal, the 10 following sequence is executed.

- 1) At some instant a signal DS_START, starts the time measurement system.
the time of DS_START has a known relation to the transmit time, and 15 must be within the body of the receive signal.
- 2) The measurement system is stopped by DS_STOP, which is the first positive going edge following a negative going edge in the receive signal.
20 By using the negative going edge to qualify the positive going edge as the stop signal, the time measurement system is always assured to have a minimum measurement time of one half period of the receive signal, thereby avoiding otherwise possible nonlinearities of the measurement system and arming logic, when measuring time intervals 25 close to zero.

Figure 3 shows four different trigger cases, 1-4. For clarity, only the digitized signals of the ultrasonic receive signal bursts (RX_UP (dashed line) and RX_DOWN) are shown. The signals shown correspond to positive flow, i.e. 30 flow in the direction where the downstream signal is faster than the upstream signal. For each of the four cases, the resulting input signal (DS_RUNUP) to the time measurement system is shown. The positive going edge of the

DS_RUNUP signal corresponds to DS_START, and the negative going edges corresponds to the DS_STOP signals generated for each up- and downstream measurement. In cases 1 - 3 the correct Δt is measured, as indicated by the Δt arrows. Taking case 1 as example, after generating the

5 send signal in the down stream direction a timer is started at time t_a (initially at the time DS_START_INI) and stopped t_b when a negative flank is followed by a positive flank in RX_DW. Now the downstream transmission time has been measured.

10 After generating the send signal in the upstream direction a timer is started at time t_a and stopped at t_c when a negative flank is followed by a positive flank in RX_UP. Now the up stream transmission time has been measured. Subtracting the downstream time from the upstream time returns a positive value of Δt . However, in case 4, the timing of DS_START results in an

15 erroneous measurement of Δt because the counter is not stopped until t_d . Δt becomes negative as indicated with the arrow pointing in the opposite direction of the arrow in case 1. Thus, as different zero crossings of the upstream and downstream signals are compared to each other, this measurement must be discarded.

20 The valid range for DS_START in the figure is denoted with letter A, and the invalid ranges are denoted with letter B. As the flow-rate increases, the A-ranges decreases, and the B-ranges increases correspondingly, leaving only the start position in case 2, as valid when the displacement between the

25 measurements has reached the maximum value of one signal period. In order to be able to distinguish between valid and invalid measurements, the span of Δt must be limited to less than the signal period, t_{sig} . The following is observed:

30 - The maximum measurement range: $\Delta t_{span} = \Delta t_{max} - \Delta t_{min} < t_{sig}$.
 - At positive flow an erroneous measurement results in a measured Δt of:

$$\Delta t_{meas} = \Delta t - t_{sig}$$

- At negative flow an erroneous measurement results in a measured Δt of:

$$\Delta t_{\text{meas}} = \Delta t + t_{\text{sig}}$$

However, when repositioning the starting time, there are som practical

5 limitations to take account of. First, the DS_START instant can only be adjusted with a minimum resolution of t_{res} as indicated in Figure 3, typically dictated by the clock resolution of a microcontroller. A typical resolution is 250 ns for a microcontroller running a 4 MHz clock speed. Second, the peak to peak timing noise, t_N , as measured on the qualifying (negative going) edge of
 10 the receive signal (RX_UP / RX_DOWN), relative to DS_START. (the noise is partly thermal noise from the circuitry, and noise induced by flow fluctuations).

This leads to the following practical constraints on the reference value:

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$$\text{At positive flow, } \Delta t > 0: \Delta t_{\text{max}} < t_{\text{sig}} - (t_{\text{res}} + t_N)$$

$$\text{At negative flow, } \Delta t < 0: -\Delta t_{\text{min}} < t_{\text{sig}} - (t_{\text{res}} + t_N)$$

Figure 4 shows the relations between Δt_{meas} , Δt_{max} , Δt_{min} , t_{res} , t_N and the true
 20 Δt . The unbroken curve corresponds to successful measurements of Δt , and the dashed curve corresponds to erroneous measurements of Δt , Δt_{error} . The boxes $t_{\text{res}} + t_N$ represents the above mentioned inequalities. Results are skipped if they are outside the limits of t_{min} and t_{max} . Considering the case of
 25 Δt_{max} as the limiting factor in Figure 4, it is seen that the limited resolution of DS_START t_{res} and the noise t_N allows for a similar amount of negative flow Δt_{min} , and vice versa. If Δt_{min} is the limiting factor, the opposite will be the case.

30 The inventive trigger scheme has three different levels of action, which all perform adjustments on the DS_START value used for the following measurement. Before each pair of upstream and downstream measurements are performed, DS_START is calculated as:

- DS_START = DS_START_INIT + L1 + L2 + L3.
- DS_START_INIT is the initial value of DS_START.
- L1, L2 and L3 are the adjustment results for each trigger level. The initial

5 value is 0.

Level 1 of the trigger scheme is the basic trigger functionality which ensures that Δt is measured on the same zero-crossing (relative to the signal start) in the upstream and downstream receive signals. The level 1 mechanism is as follows: If Δt_{meas} is outside the interval $[\Delta t_{min} ; \Delta t_{max}]$, L1 is incremented in steps of T_{res} , following the sequence: $L1 = (0-1-2 \dots (n-1)-0-1-2\dots) \times T_{res}$, where $n = \text{round}(T_{sig}/T_{res})$. I.e. L1 sweeps one period T_{sig} of the receive signal. W

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15 The consequence of using only level 1 of the trigger is that, as the time of flight varies with media temperature, the signal zero-crossing used for measurement changes.

Level 2 of the trigger is only invoked after passing level 1 without

20 adjustments. The purpose of level 2 is to keep the average time from DS_START to DS_STOP (i.e. DS_RUNUP) constant within the limits given by T_{res} . By choosing T_{sig} as the target time for the average value of DS_RUNUP, The starting point DS_START is kept in the optimal position (corresponding to case 2 in figure 1), where the distance in time to the error

25 trig ranges B is as long as possible.

25

30 The level 2 mechanism is as follows: Calculate the average of the measured upstream and downstream DS_RUNUP times. If the average DS_RUNUP differs from T_{sig} by more than $\pm T_{adj}$, L2 is adjusted up or down accordingly, in steps of T_{res} . The limit for adjustment T_{adj} is based upon T_{res} , and should be bigger than $T_{res}/2$, because an adjustment smaller than t_{res} in unwanted manner would increase the distance to the optimal point.

With the level 2 part of the trigger scheme implemented, the trigger point will track the received signal, as long as there are no signal drop-outs. To be able to track the signal in all cases, the third level of the trigger is invoked:

5 Level 3 of the trigger is only invoked after passing level 2 without
adjustments. The purpose of level 3 is to track a certain zero-crossing in the
receive signal, at all media temperatures. The measured media temperature
and the relation of sound speed to media temperature, is used to calculate
the expected average transmission time from transmit to receive.

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The level 3 mechanism is as follows: The directly measured average
transmission time (DS_START + DS_RUNUP - SIGNAL_OFFSET(*)) is
compared to the expected transmission time from the temperature
measurement. If the comparison is outside the limits of $\pm t_{sig}/2$, L3 is adjusted

15 up or down accordingly, in steps of t_{sig} .

(*) SIGNAL_OFFSET is the distance from the receive signal start to
preferred signal zero-crossing).

20 Besides the result of tracking a constant zero-crossing in the signal, level 3
gives the extra benefit, that it is now possible to use the measured
transmission time in the flow calculation instead of using the transmission
time measured indirectly via temperature. This allows the temperature
measurement to be rather crude without inflicting the flow measurement. A
flow chart describing the three levels is found in figure 5.

25 Figure 6 is a block diagram of the preferred embodiment 14 of an ultra sonic
flow meter. A generator 4 generates an exitation pulse for a front end 5. To
this circuit ultra sonic transducers 3 are connected. From front end 5 the ultra
sonic receive signals are passed to a comparator 6, which converts the
analog signals into digital signals. A first flip flop 7 and a second flip flop 8
30 receives the digital pulses. The second flip flop 8 is armed by the output of
the first flip flop, and the first flip flop 7 is armed by the signal DS_START

coming from an arming logic 13 placed in a microcontroller 14. Inputs to the arming logic is the difference time Δt , two transmission times (t_1, t_2) and the media temperature. The difference time and the transmission times are fed from a time measurement circuit 10, which measures the width of

5 DS_RUNUP, which is the difference between the starting signal DS_START and the stopping signal DS_STOP. DS_STOP (negated) is the output of the second flip flop 8 and fed to AND circuit 9. Box 12 shows the set of parameters that are used in the arming logic for the generation of the starting time DS_START. Track select 15 selects the set of transducers to use.

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Due to the low Δt unbalances in the generation of the upstream and downstream signals must be avoided. Such differences may occur if two different electronic send and receive circuits are used, where component tolerances cause differences in the group run time of the signals. Even small

15 differences will have a huge error impact on ultra sonic systems using small Δt . In order to overcome this problem a circuit as described in DE 100 48 959 A1 is used as front end 5. This circuit uses one and the same electronic components for send and receive, thus neither component tolerances nor temperature differences influence on Δt .

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The span of the typical reference band in this embodiment is -20 ns up to 600 ns. If the measured Δt falls outside of this span, the measurement is skipped.

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Claims

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1. Method for measuring flow by means of an ultra sonic flow meter, where a transmission of an ultra sonic signal is made in an upstream and a downstream direction and where a time measurement is initiated at a starting time upon receipt of the ultra sonic signal and stopped at a stopping time **characterized in** that a first series of transmissions are made where the starting time in each transmission is incremented or decremented until a time difference (Δt) between the upstream and downstream signal is inside a reference band (Δt_{span}), whereafter a calculation of the flow based on the time measurements is done.
2. Method according to claim 1 **characterized in** that a second series of transmissions following the first transmissions is made, where the starting time in each transmission is incremented or decremented until the time period (DS_RUNUP) between the starting time (DS_START) and the stopping time (DS_STOP) is approximately equal to a multiplum of half the time period of the ultra sonic signal, but preferably equal to the time period.
3. Method according to claim 2 **characterized in** that a third series of transmissions follows the first and second series, and that the starting time in the third series of transmissions is incremented or decremented until a difference between a calculated average transmission time and a transmission time reference value determined on the basis of the media temperature is inside a reference band.
4. Method according to claim 3 **characterized in** that incrementation or decrementation during the third series of transmissions is done in steps of a timely resolution (t_{sig}) that is approximately equal to the period of the received signal.

5. Method according to claim 1 characterized in that incrementation or decrementation is done in steps of a timely resolution (t_{res}) defined by the resolution of the mikrocontroller.

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6. Method according to claim 1, 2 or 3 characterized in that, following the starting time, the time measurement is stopped at the first positive zero crossing of the received ultra sonic signal or at the first negative zero crossing.

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7. Method according to claim 1, 2 or 3 characterized in that, following the starting time, the time measurement is stopped at the first positive zero crossing following a negative zero crossing of the received ultra sonic signal, or vice versa.

15

8. Method according to claim 1 characterized in that the starting time in the first transmission in the first series of transmissions is a fixed value (DS_START_INI).

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9. Method according to claim 1 characterized in that the reference band (Δt_{span}) is delimited by a maximum difference time (Δt_{max}) and a minimum difference time (Δt_{min}), the width of the band being smaller than the time period (t_{sig}) of the ultra sonic receive signal.

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10. Method according to claim 9 characterized in that a safety margin is added to the reference band, the safety margin corresponding to at least the timely resolution (t_{res}) of the incrementing or decrementing steps, and preferably the sum of a resolution and the duration of a timing noise (t_N).

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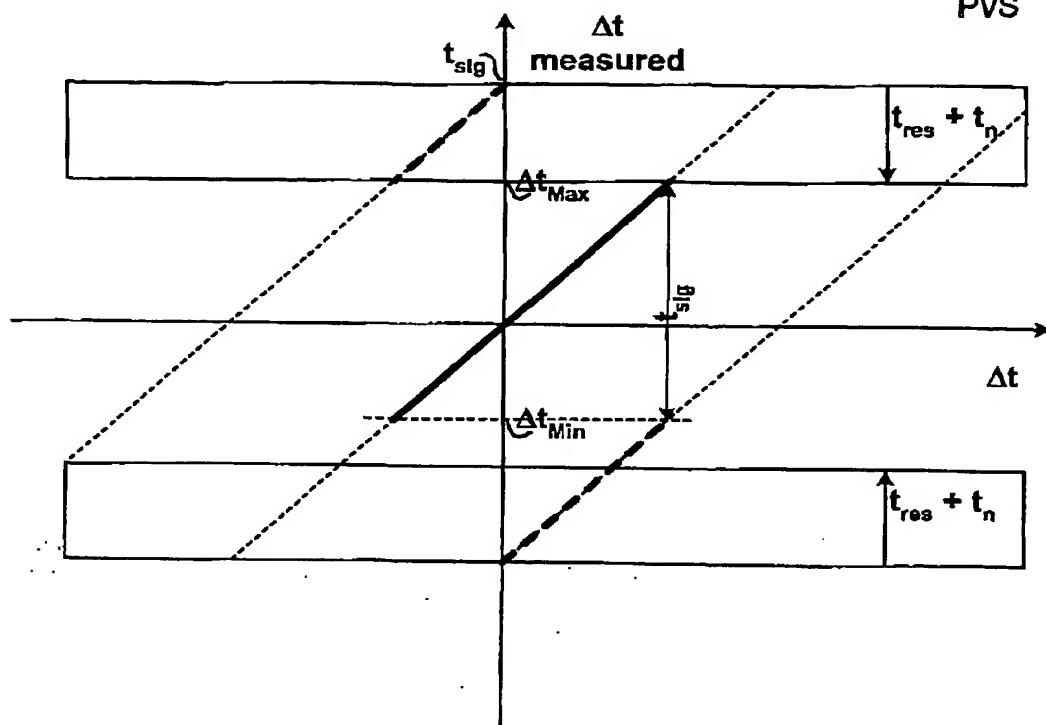


Fig. 4

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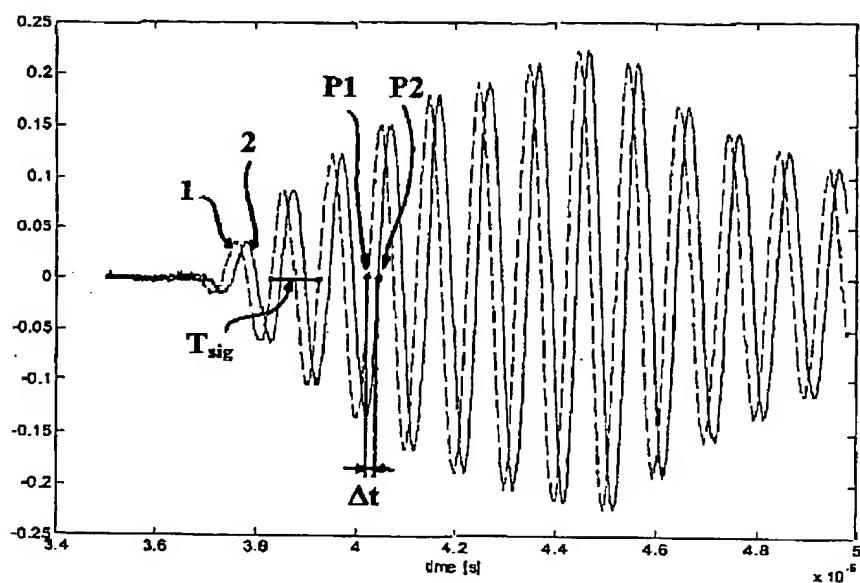


Fig.1

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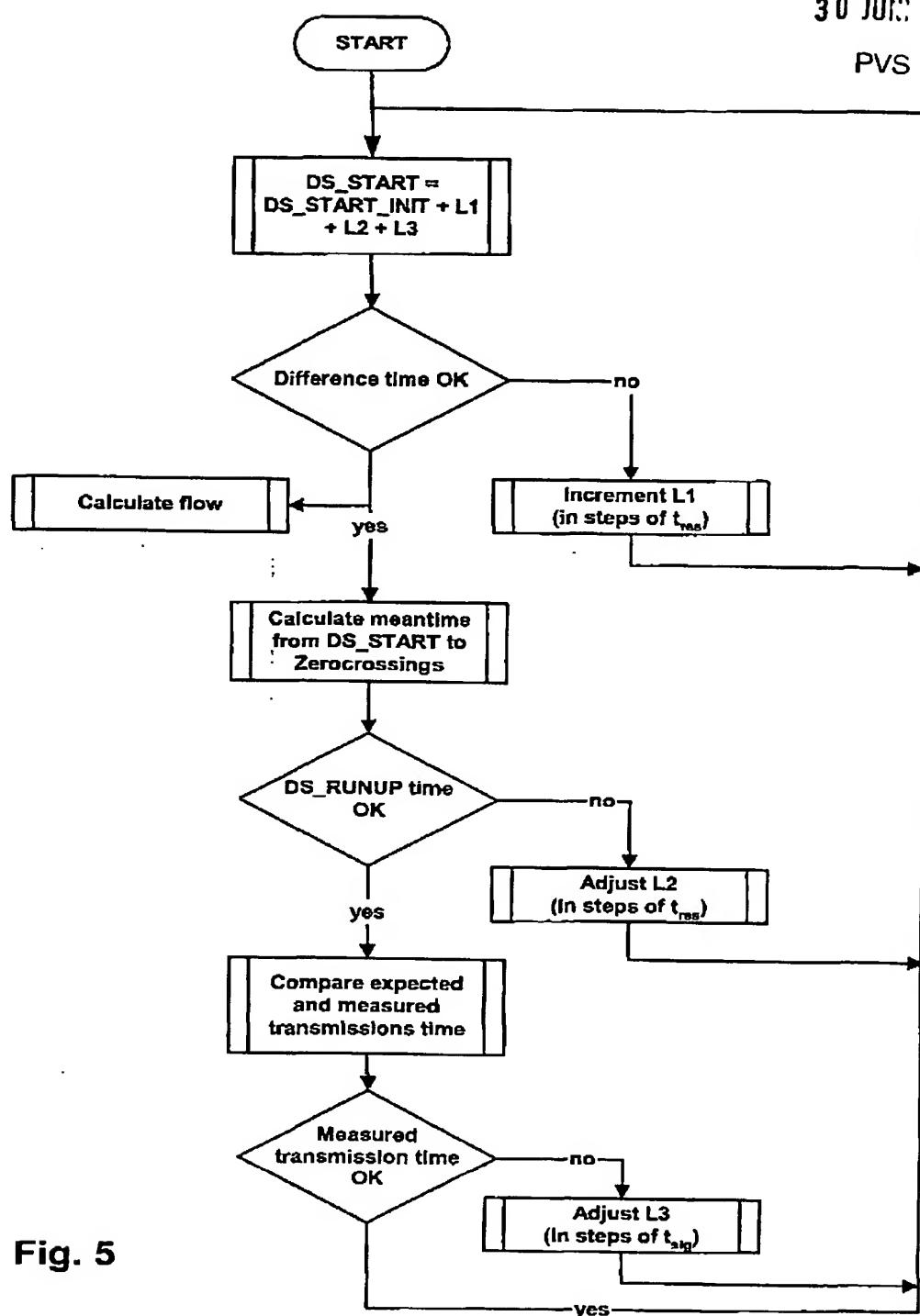


Fig. 5

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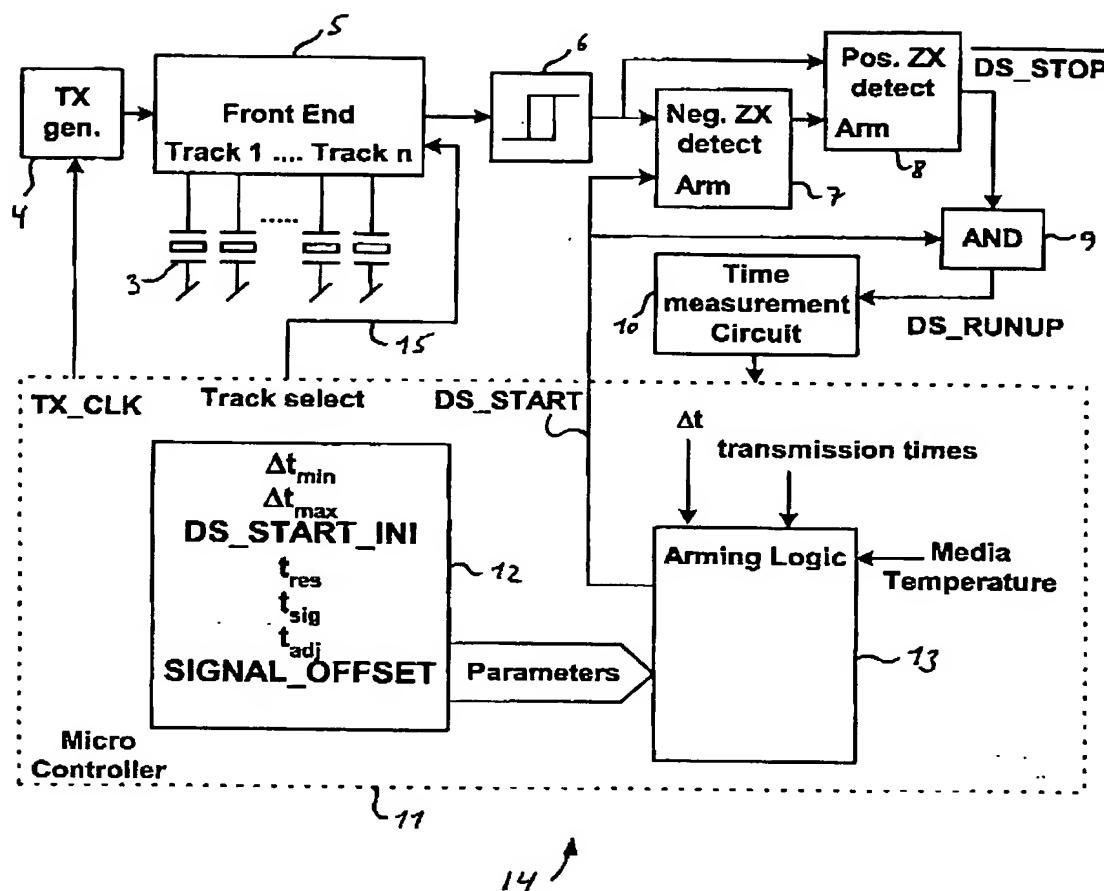


Fig. 6

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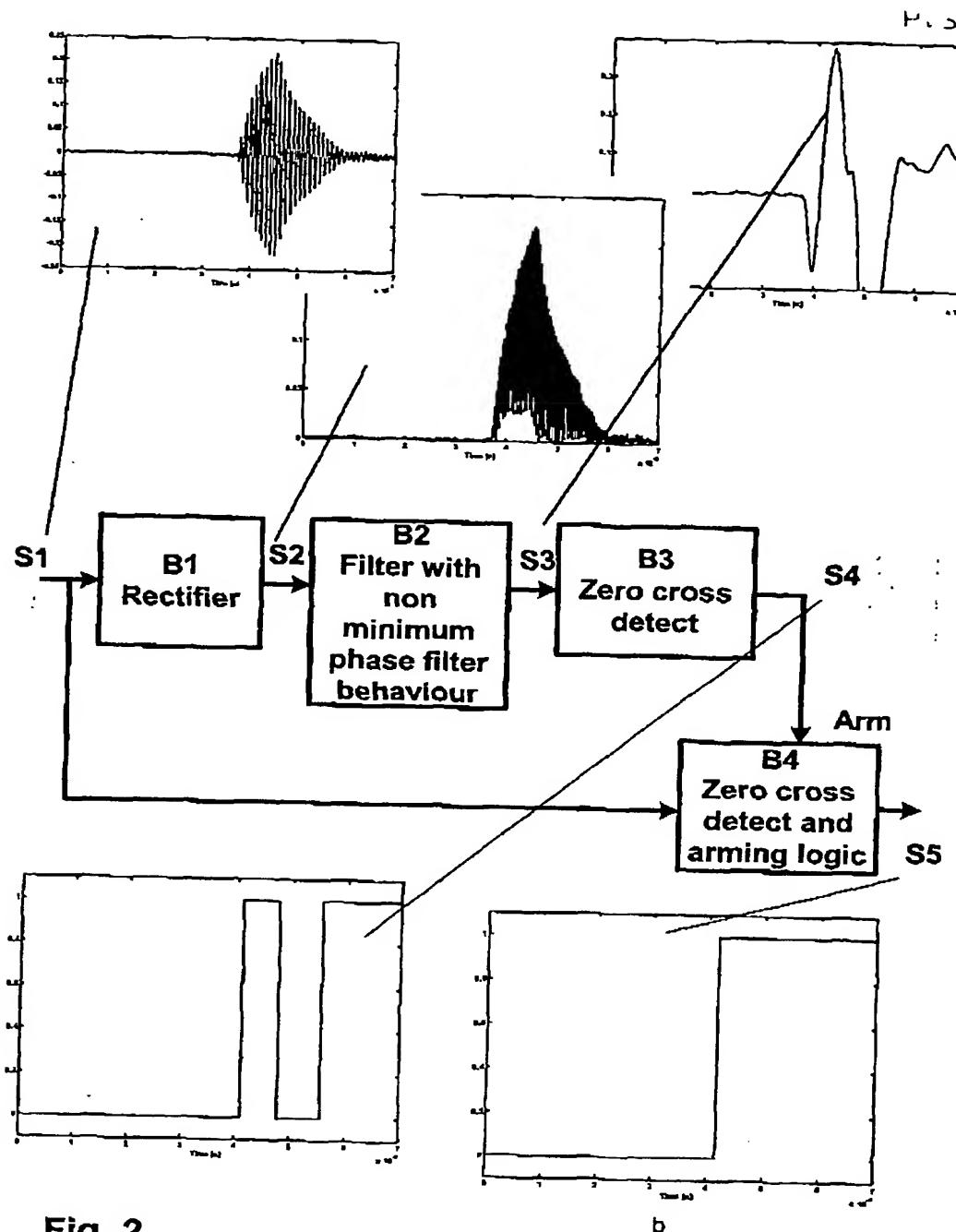


Fig. 2